

## FABRICATION OF MOUNTING BRACKET USING GLASS FIBER AND EPOXY COMPOSITES

Jaya kumar.V<sup>1</sup>Balaji. H<sup>2</sup>Elumalai E S<sup>3</sup>

<sup>1,2</sup> Assistant Professor Department of Aeronautical Engineering, Tagore Engineering College,  
Anna University Chennai, Tamilnadu

<sup>1</sup>jaikumar.v16@gmail.com, <sup>2</sup>balajihk007@gmail.com

<sup>3</sup> Assistant Professor Department of Aeronautical Engineering, Hindustan Institute of Science  
and Technology, Chennai, Tamilnadu, elu529@gmail.com

**Abstract**—This paper reviews some of the advances that have been made in stress analyses of the mounting brackets of aircraft component. Finite Element Analysis is implemented to calculate stress-intensity factors precisely for finding pits in structures. Observations of small-crack behavior at open and rivet-loaded holes and the development of small-crack theory have led to the prediction of stress-life performance for components with stress concentrations under aircraft spectrum loading. By using the technique called crack-closure concept crack growth can be easily monitored in the aircraft structures. These advances are helping to assure continued safety of aircraft structures the main motivation is that to increase the life of the material used for mounting brackets for structural application. i.e. increases the No. of cycles to failure (Nf) of the material.

Key Words: Mounting Bracket, glass fibre, epoxy resin, rivet-loaded holes, crack growth, fatigue life.

### 1. INTRODUCTION

Fatigue was a major criterion in Aircrafts and other structural industry because of its nature to decrease the life span of components. [1].with the help of modern computer technologies we easily predicted the stress dominant factors on 3D cracks in a realistic manner. [2].

Therefore fabrication of fatigue and corrosion less structures is impossible nowadays even though with modern techniques. But the improvement in design, computational analysis increases the life span of the component. [3] This presentation is focused on such methods with special emphasis on practical fatigue reliability considerations.[4] All structures or components have traditionally been designed using time based structural and fatigue analysis methods. By fatigue analysis approach, optimized stress design be achieved in an effective manner.[5]Therefore with this technique we had many advantages like empathetic the fatigue nature and analysis the detailed 3D structures instead of simplified 2D structures. [6]

Basically composite be made up of, primary strengthen fibers and binding resin matrix with some additives. Wood and bone are natural composite materials: wood consists of cellulose fibers in aligning matrix and bone consists of hydroxyapatite particles in a collagen matrix. [7]Frequently used composites in aircraft industries are glass-fiber-reinforced plastic and sometimes with carbon for better strength which involve both carbon and glass fibres, both of which are stiff and strong (for their density),[8] but brittle, in a polymer matrix, which is tough but neither particularly stiff nor strong. [9].

Almost Every structures are designed with respect to time centered and fatigue analysis methods. But with the help of frequency based fatigue analysis approach, the stress and strain response related to the applying load be found out and easily predict the optimized fatigue life and has many advantages over other methods of predicting the potentially inadequate simplified version and, and more computationally efficient fatigue analysis procedure. [10] For considering the popular engineering difficulties, loading to the structures places the top position with respect of the design.[11]These problems be overruled by knowing the Gaussian approach of deforming. Fortunately, most engineering processes conform reasonably well to these assumptions.[12]

The starting point for any fatigue analysis is the response of the structure or component, which is usually expressed as a stress or strain time history. [13]By referring S-N diagram, a stress and strain cycle of fatigue design was made. However, because real signals rarely conform to this ideal constant amplitude situation, an empirical approach is used for calculating the damage caused by stress signals of variable amplitude. [14]

## 2. DESCRIPTION

Fatigue was a major factor to consider while designing any component. Basically three test were to conducted with different fabrication criteria and the composition of fibers and resin. Here for all the four fabrications same fibers and resins are used with different composition and orientations.

### TECHNIQUES USED:

Fatigue test can be done by various methods.

1. Tensile fatigue test.
2. Compression fatigue test.
3. Shear fatigue test

### Mounting Bracket Design

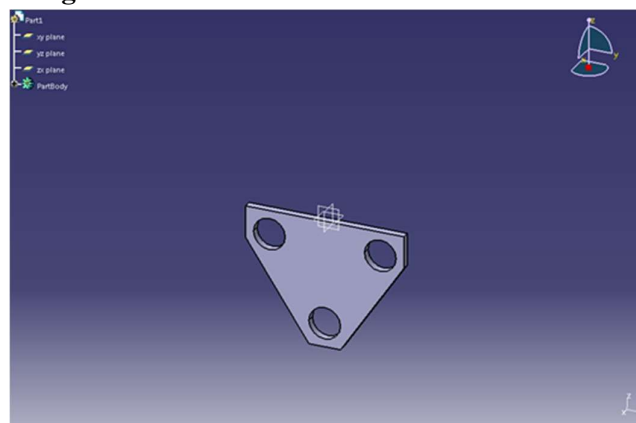


Fig 2.1: CATIA model of mounting brackets for structural assembly

## 3. PERFORMANCE ANALYSIS

The mounting brackets that are manufactured by Glass fibre (10 MIL E-Glass) and Epoxy resin (Araldite 257) to analyse the fatigue life.

### For laminate 1

Specifications of material:

- No. of Lamina (Plies) in a specimen = 08
- Name of the Material = 10 MIL E – Glass
- Name of the Resin = Araldite GY 257
- Name of the Hardener = C2963
- Specimen Dimension = 150 x 150 mm
- Specimen Thickness = 2 mm.

Fabrication of mounting brackets and Preparation of test specimen for laminate 1



Fig.3.1 Fabrication of mounting brackets

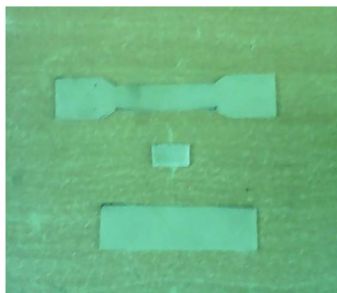


Fig. 3.2 Before test

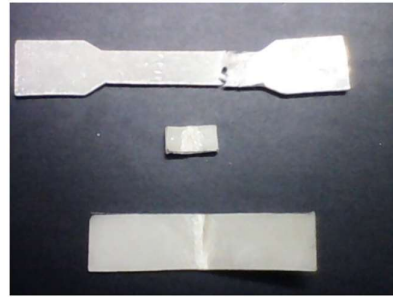


Fig.3.3 After test

3.2.1.4 Test results for laminate 1

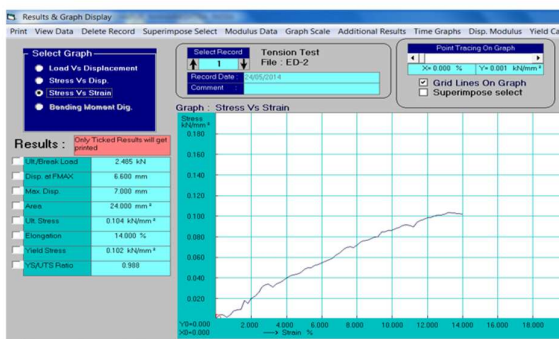


Fig 3.4 Tensile test for a laminate 1.



Fig 3.5 Flexural test for a laminate 1.

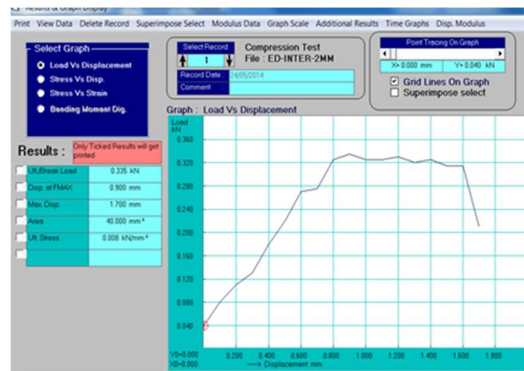


Fig 3.6 ILSS test for a laminate 1.

For laminate 2

Specifications of material:

- No. of Lamina (Plies) in a specimen = 12

Name of the Material = 10 MIL E – Glass  
 Name of the Resin = Araldite GY 257  
 Name of the Hardener = C2963  
 Specimen Dimension= 150 x 150 mm  
 Specimen Thickness = 3 mm

Fabrication of mounting brackets and Test piece preparation for laminate 2

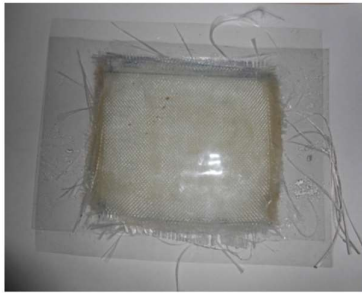


Fig.3.7 Fabrication of mounting brackets

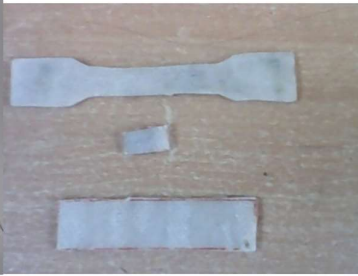


Fig 3.8 Before test

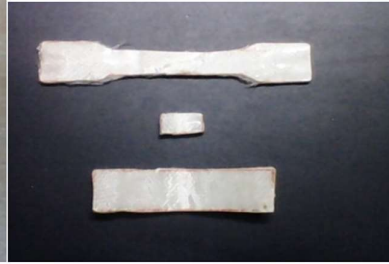


Fig 3.9 After test

Test results for laminate 2

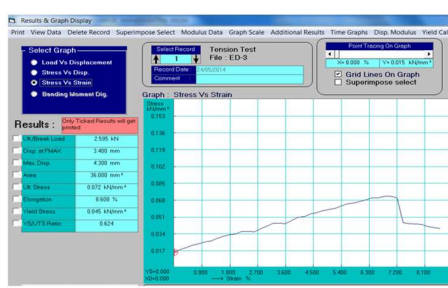


Fig 3.10 Tensile test for an laminate 2.

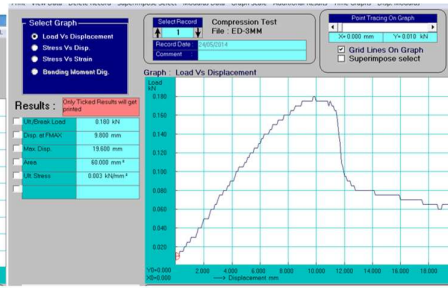


Fig 3.11 Flexural test for an laminate 2.

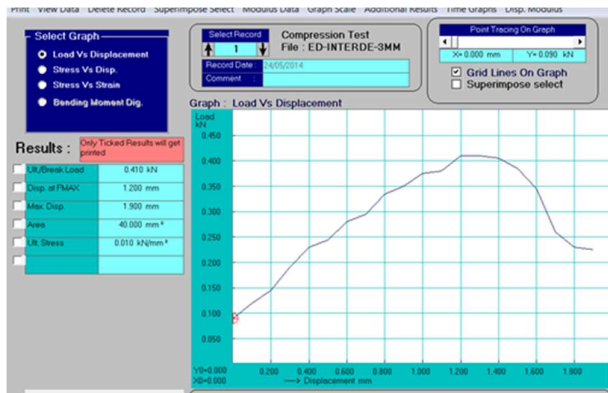


Fig 3.12 ILSS test for an laminate 2.

For laminate 3

Specifications of material:

No. of Lamina (Plies) in a specimen = 20  
 Name of the Material = 10 MIL E – Glass  
 Name of the Resin = Araldite GY 257  
 Name of the Hardener = C2963

Specimen Dimension = 150 x 150 mm

Specimen Thickness = 5 mm

Fabrication of mounting brackets for laminate 3



Fig.3.13 Fabrication of mounting brackets.



Fig 3.14 Debagging of laminate 3

Test piece preparation for laminate 3



Fig 3.15 Before testing



Fig 3.16 After testing

Test results for laminate 3

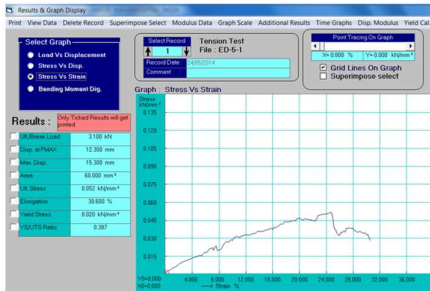


Fig 3.17 Tensile test for an laminate 3.

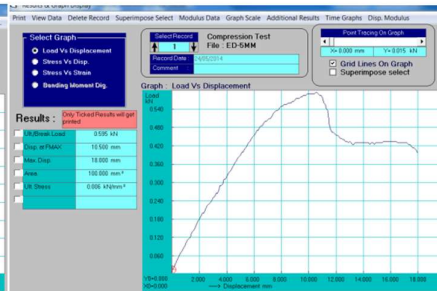


Fig 3.18 Flexural test for an laminate 3.

**For laminate 4**

**Specifications of material:**

No. of Lamina (Plies) in a specimen = 20 (Cross ply orientation).

Name of the Material = 10 MIL E – Glass

Name of the Resin = Araldite GY 257

Name of the Hardener = C2963

Specimen Dimension = 150 x 150 mm  
 Specimen Thickness = 5 mm

Laminate preparation for laminate 4

Test results

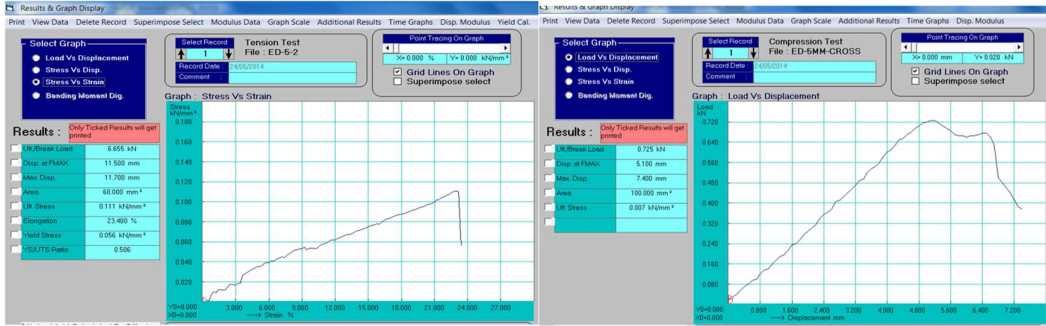


Fig 3.21 Tensile test for a laminate 4.

Fig 3.22 Flexural test for an laminate 4.

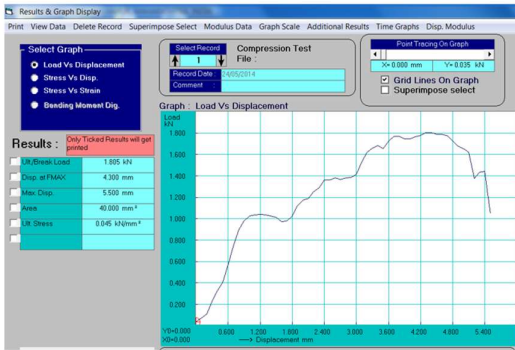


Fig 3.23 ILSS test for a laminate 4.

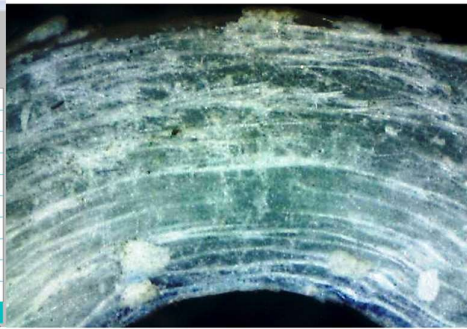


Fig 3.24 Macroscopic image of ILSS test

Mounting Bracket



Fig 3.25 Mounting bracket

4. FORMULA USED TO FIND NO. OF CYCLES TO FAILURE:

$$\frac{\Delta \epsilon_{eq}}{2} = \frac{\sigma_f' - \sigma_m}{E} (2N_f)^b + \epsilon_f' (2N_f)^c$$

b = - 0.067 (Shear fatigue strength exponent)

c = - 0.500 (Shear fatigue ductility exponent)

$\sigma_f' = 0.8$  KN/mm<sup>2</sup> (Fatigue strength coefficient)

$S_y = 0.4$  KN/mm<sup>2</sup> (Material yield stress)

$S_u = 0.501$  KN/mm<sup>2</sup> (Material ultimate stress)

$\epsilon_f' = 0.009$  (Fatigue strain coefficient)

$K' = 0.81$  KN/mm<sup>2</sup> (Cyclic strength coefficient)

E = 5 KN/mm<sup>2</sup> (Young's modulus)

Properties of Glass Epoxy:

Density = 2.1 g/cm<sup>3</sup>

Longitudinal modulus E1 = 60GPa

Transverse modulus E2 = 13GPa

Shear modulus G12 = 3.4GPa

Poisson ratio = 0.3

4.3. Model calculation:

$$\epsilon = \Delta/l = 11.70/120 = 0.0975$$

So,

$$0.0975/2 = 800 - 111/5000 \times (2N_f)^{-0.067} + 0.009 \times (2N_f)^{-0.5}$$

Then,

$$0.03 = 0.1378 \times 0.955 (N_f)^{-0.067} + 0.009 \times 0.707 (N_f)^{-0.5}$$

$$0.0048 = 132 \times 10^{-3} (N_f)^{-0.067} + 6.363 \times 10^{-3} (N_f)^{-0.5}$$

$$N_f = 3.017 \times 10^6 (\text{cycles})$$

Summary:

Fatigue life of the SAE 1045 steel is

$$N_f = 0.1449 \times 10^3 (\text{cycles})$$

Fatigue life of the mounting bracket (Glass fibre (10 MIL E-Glass) and Epoxy resin (Araldite 257) for 5mm (cross ply laminate) is

$$N_f = 3.01 \times 10^6 (\text{cycles})$$

## 5. CONCLUSION:

No. of cycle to failures for the fatigue analysis of mounting brackets by using composite materials has been increased. This project explains about the Fatigue analysis of Mounting Brackets. The No. of cycles to failure of the composite material [Glass fibre (10 MIL E-Glass) and Epoxy resin (Araldite 257)] for mounting brackets has been increased by changing the thickness and the orientations of fibre.

## REFERENCES

1. J. C. Newman, Jr "Advances in fatigue and fracture mechanics analyses for aircraft structures" Mechanics and Durability Branch, NASA Langley Research Center, Hampton, VA, USA 23681

2. Stevan Maksimović, PhD (Eng)1) “Fatigue Life Analysis of Aircraft Structural Components” Scientific-Technical Review, Vol. LV, No. 1, 2005.
3. Ulf G. Goranson “Fatigue issues in aircraft maintenance and repairs” Boeing Commercial Airplane Group, Seattle, WA, USA (Received 10 February 1997).
4. Swift, T., “Damage Tolerance in Pressurized Fuselage,” 11th Plantema Memorial Lecture, 14th Symposium of the International Committee on Aeronautical Fatigue (ICAF), New Materials and Fatigue Resistant Aircraft Design, Ottawa, Canada, June 8-12, 1987.
5. Shivakumar, K. N. and Newman, J. C., Jr., “ZIP3D – An Elastic and Elastic-Plastic Finite-Element Analysis Program for Cracked Bodies,” NASA TM-102753, November 1990.
6. Young, R. D.; Rouse, M.; Ambur, D. R. and Starnes, J. H., Jr., “Residual Strength Pressure Tests and Nonlinear Analyses of Stringer- and Frame-Stiffened Aluminum Fuselage Panels with Longitudinal Cracks,” The Second Joint NASA/FAA/DoD Conference on Aging Aircraft, C. E. Harris, ed., NASA CP-208982, 1999, pp. 408-426.
7. Furuta, S.; Terada, H. and Sashikuma, H., “Fatigue Strength of Fuselage Joint Structures under Ambient and Corrosive Environment,” Fatigue in New and Ageing Aircraft, R. Cook and P. Poole, eds., EMAS, Ltd., 1997, pp. 231-249.
8. Newman, J. C., Jr.; Phillips, E. P. and Swain, M. H., “Fatigue-Life Prediction Methodology using Small-Crack Theory,” International Journal of Fatigue, Vol. 21, 1999, pp. 109-119.
9. Phillips, E. P., “The Influence of Crack Closure on Fatigue Crack Growth Thresholds in 2024-T3 Aluminum Alloy,” Mechanics of Fatigue Crack Closure, ASTM STP 982, J. C. Newman, Jr. and W. Elber, eds., American Society for Testing and Materials, Philadelphia, PA, 1988, pp. 505-515.
10. Swain, M. H.; Everett, R. A.; Newman, J. C., Jr. and Phillips, E. P., “The Growth of Short Cracks in 4340 Steel and Aluminum-Lithium 2090,” AGARD R-767, 1990, pp. 7.1-7.30.
11. N.W.M. Bishop and Hu Zhihua, The Fatigue Analysis of Wind Turbine Blades Using Frequency Domain Techniques, European Wind Energy Conference, EWEC '91, Amsterdam, 246-250, (1991).
12. port, T. & A. M. Report No. 379, Department of Theoretical and Applied Mechanics, University of Illinois, Urbana, January 1974.
13. TOPER, T.H., WETZEL, R.M., and MORROW, J.: Neuber's rule Applied to Fatigue of Notched Specimens, Journal of Materials, 1969, Vol.4, No.1.
14. Miller, M., Luthra, V. K. and Goranson, U. G., Fatigue crack growth characterization of jet transport structures. 14th Symposium of the International Committee on Aeronautical Fatigue (ICAF), Ottawa, Canada, June 8–12, 1987.
15. Swift, T., Damage tolerance in pressurized fuselages. 11th Plantema Memorial Lecture, 14th Symposium of the International Committee on Aeronautical Fatigue (ICAF), Ottawa, Canada, June 8–12, 1987.
16. Goranson, U. G. and Miller, M., Aging jet transport structural evaluation programs. 15th Symposium of the International Committee on Aeronautical Fatigue (ICAF), Jerusalem, Israel, June 21–23, 1989.